

## Influence of Multi Anti – Reflective Layers on the Silicon Solar Cells

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### ABSTRACT

The deposition of an antireflection coating (ARC) is an efficient way to ensure low reflectivity of silicon photovoltaic cells. With an ARC, the zero reflectivity takes place only for a given wavelength since this layer acts as a quarter-wave plate. The application of a double antireflective coating (DARC) combining the deposition of two layers on the front of the cell is a way to improve the reflection properties on the conversion efficiency [1]. This work tries to find the better configuration of the double anti-reflective layers to effectively improve the electrical performance of the silicon solar cells [2].

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### Introduction

The reflection of the incident photons on the interface of substrates is an important source of losses for photovoltaic conversion, in addition to those transmitted through the cell without being absorbed.

For mass production of solar cells, more efficient solutions must be found to limit photons lost at the front of the cell. The idea is to make the deposition of one or more anti-reflective layers.

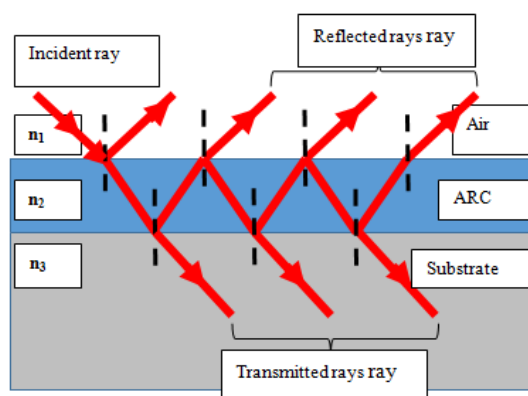
For that, the hydrogenated silicon nitride SiN<sub>x</sub>:H (SiN) and silicon oxide SiO<sub>x</sub>:H are interesting materials since they can act as anti-reflection coating due to their low absorption and their adjustable optical properties [3].

### Experimental

#### Theory

##### Study of a Single Anti-reflective Coating

Figure 1 shows the configuration of a substrate material coated by an anti-reflective coating of refractive index  $n_2$ .



**Figure 1:** Incident reflected and transmitted light radiations through three different refraction indices environments

Incident light ray is falling on the top the ARC and is submitted to multiple reflection and transmission on both air-ARC and ARC-substrate interfaces. The incident wave is defined by the maximum amplitude of the electric field  $E_0$ .

The path difference between two consecutive reflected rays is:

$$\delta = 2e n_2 \cos i_2 \quad (1)$$

where  $e$  is the ARC thicknesses,  $i_2$  the refractive angle. The corresponding phase difference is:

$$\Delta\varphi = \frac{2\pi\delta}{\lambda} \quad (2)$$

The resulting amplitude  $E_r$  of reflected electric field is expressed in terms of  $E_0$ ,  $r_{12}$ ,  $r_{23}$ ,  $t_{12}$ ,  $t_{21}$  and  $\Delta\varphi$ :

$$E_r = E_0 \left[ r_{12} + \frac{t_{12} r_{23} t_{21} e^{j\Delta\varphi}}{1 - r_{23} r_{21} e^{j\Delta\varphi}} \right] \quad (3)$$

The reflection coefficients  $r_{ij}$  and the transmitted ones  $t_{ij}$  ( $i, j = 1, 2, 3$ ) are given by Fresnel formulas, in the case where the electric field  $E_0$  is perpendicular to the incidence plane. For destructive interferences, the amplitude condition is  $E_r = 0$  and the phase condition is  $\Delta\varphi = \pi$ , thus giving  $e = \frac{\lambda}{4n_2}$ . Under these conditions, equation (3) gives:

$$r_{12} - \frac{t_{12} r_{23} t_{21}}{1 + r_{23} r_{21}} = 0 \quad (4)$$

The phase condition for the optimum thickness and the refractive index of the antireflection layer is:

$$e = \frac{\lambda}{4n_2} \quad (5)$$

Losses caused by the reflection on solar cells without antireflection layer are important and have a significant impact on cell photocurrent. It is interesting to minimize these losses by growing simple or multiple anti-reflective coatings on solar cells. The improvement provided by a high refractive index of the ARC for high photons energy may be attenuated by the increase of absorption of light in the anti-reflective coating. It is appropriate from these

elements to not considering only the reflection, but also the absorption coefficient of the thin layer coating. Accordingly, it is convenient to use, in the case of an ARC, a SiN layer with a refractive index slightly lower than 2 so to obtain a maximum of radiation transmitted [4].

### Study of Multi antireflective Coating

Multilayer antireflections coating (MARC) are simulated using a «Matrix method» [5]. This method allows to deal with multiple anti-reflective layers of different materials as shown in Fig. 2.

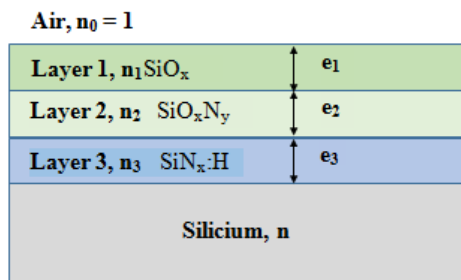


Figure 2: Example of multiple anti-reflective coatings

As indicated in figure 3, the method is based on a stack of  $p$  thin layers with different refractive indexes  $n_1, n_2, \dots, n_p$  with respective thicknesses  $e_1, e_2, \dots, e_p$  placed on a substrate of refractive index  $n_s$ . The incident ray propagates with an amplitude  $E_0$  and incident angle which is between 0 and  $65^\circ$ .

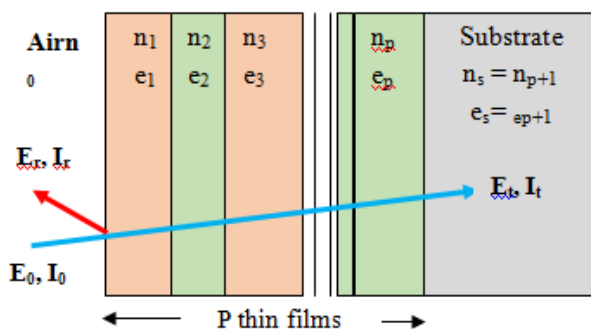


Figure 3: A stack of thin films coating an active substrate for solar cell

The total amplitude  $E_r$  of the reflected radiations and the total ones  $E_t$  transmitted by the several layers are obtained using the following relation. 6 is the product of all amplitudes of radiations crossing through the layers and the diopeters separating two layers.

$$\begin{pmatrix} E_r \\ E_0 \end{pmatrix} = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} \begin{pmatrix} 0 \\ E_t \end{pmatrix} = M \begin{pmatrix} 0 \\ E_t \end{pmatrix} \quad (6)$$

The matrix  $M$  can be written as:

$$M = D_0.C_1.D_1.C_2.....C_p.D_p \quad (7)$$

The quantity  $D_i$  is the matrix associated to the two layers  $i$  and  $i + 1$ :

$$D_i = \begin{pmatrix} \frac{n_i + n_{i+1}}{2n_i} & \frac{n_i - n_{i+1}}{2n_i} \\ \frac{n_i - n_{i+1}}{2n_i} & \frac{n_i + n_{i+1}}{2n_i} \end{pmatrix} \quad (8)$$

The path difference for radiation crossing the layer  $i$  is given by:

$$C_i = \begin{pmatrix} e^{-j\varphi_i} & 0 \\ 0 & e^{+j\varphi_i} \end{pmatrix} \quad (9)$$

The phase angle is:

$$\varphi_i = \frac{2\pi n_i e_i}{\lambda}$$

The reflection and transmission coefficients in amplitude are given by:

$$r = \frac{M_{12}}{M_{22}}; t = \frac{1}{M_{22}} \quad (10)$$

The ones in intensity are:

$$R = r \cdot r^* \quad T = t \cdot t^* \quad (11)$$

## Results and Discussion

The first approach is to use a double anti reflective coating (DARC) with two materials with different refractive indexes. Table 1 shows the materials used to make computer simulations.

Table 1: Materials used in the simulations as ARC and their refractive indexes [6]

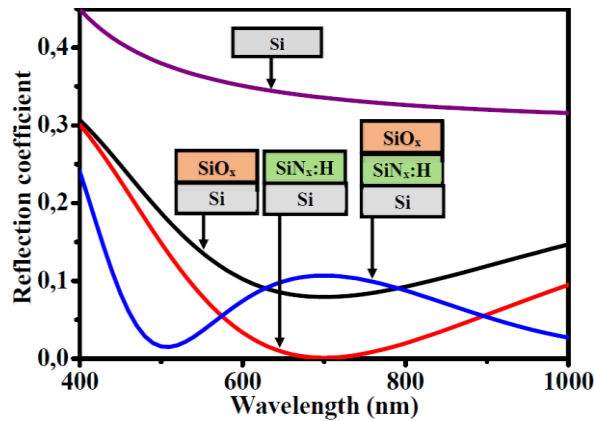
Materials	Refractive index
SiO <sub>x</sub>	$n_1 : 1,45 \sim 1,50$
SiO <sub>x</sub> N <sub>y</sub>	$n_2 : 1,50 \sim 1,80$
SiN <sub>x</sub> :H	$n_3 : 1,80 \sim 3,00$
Si	3,75

The appropriate materials in physical and technological point of view are SiN<sub>x</sub>:H, SiO<sub>x</sub>N<sub>y</sub> and SiO<sub>x</sub>. Double anti-reflection layers are realized in many works with different materials like SiO<sub>2</sub>/Si<sub>3</sub>N<sub>4</sub>, SiO<sub>2</sub>/TiO<sub>2</sub> and ZnS/MgF<sub>2</sub>[7]. However, some of these works are focused on the way to optimize these multilayers anti-reflective coating.

In the following, are presented the results obtained from the simulations of double and multi-layer reflective coatings on silicon substrate. The silicon oxide SiO<sub>x</sub> is appropriate to minimize optical losses in PV silicon cells because the minimum reflectivity was found for small optical index [8].

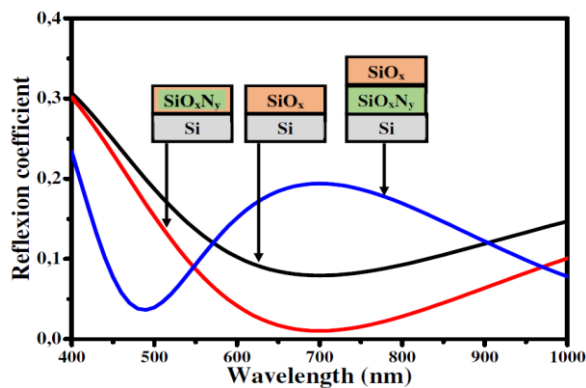
The hydrogenated silicon nitride (SiN<sub>x</sub>:H), combined with proper texturing [9], has interesting optical properties with refractive index varying between 1.8 and 3.0 with a low absorption coefficient [10]. It is first deposited on silicon substrate and provides good passivation.

Figure 4 shows the reflection coefficient as a function of incident light wavelength for a silicon substrate coated at different configurations: SiO<sub>x</sub>/Si, SiN<sub>x</sub>:H/Si and SiO<sub>x</sub>/SiN<sub>x</sub>:H/Si.



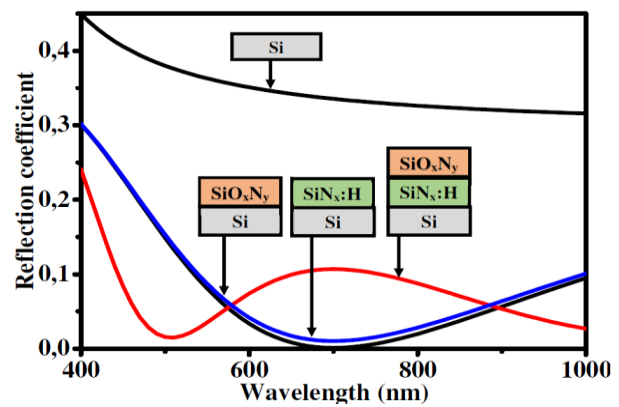
**Figure 4:** Reflection coefficient of silicon substrate with different anti-reflective coatings. The ARC thicknesses are calibrated for a wavelength  $\lambda = 700$  nm. The refractive indexes are  $n(\text{SiO}_x) = 1.45$ ;  $n(\text{SiNx:H}) = 2$ ;  $n(\text{Si}) = 3.75$

It is noted the high reflection coefficient of silicon varying from 45% to 30% from 400 to 1000 nm. The reflectivity is lowered from 30% to 12% in this wavelength range when silicon substrate is coated with a  $\text{SiO}_x$  thin film. A minimum of 8% is obtained at 700 nm corresponding to a better transmission of photons flux. For a  $\text{SiNx:H/Si}$  configuration, the reflectivity lies between 30 to 8% with a zero reflectivity at 700 nm. The blue curve shows the reflectance of  $\text{SiO}_x/\text{SiNx:H/Si}$  which is a DARC on silicon substrate. Two minima nearly zero reflectance appear at 500 nm and 1000 nm with a maximum of 10% at 700 nm, showing that the single antireflecting layer  $\text{SiNx:H/Si}$  has a better performance than the ones for  $\text{SiO}_x/\text{Si}$  and for DARC  $\text{SiO}_x/\text{SiNx:H/Si}$  especially at the calibrated wavelength.



**Figure 5:** Reflection coefficient of silicon substrate with different anti-reflective coatings. The ARC thicknesses are calibrated for a wavelength  $\lambda = 700$  nm. The refractive indexes are  $n(\text{SiO}_x) = 1.45$ ;  $n(\text{SiO}_x\text{Ny}) = 1.75$ ;  $n(\text{Si}) = 3.75$

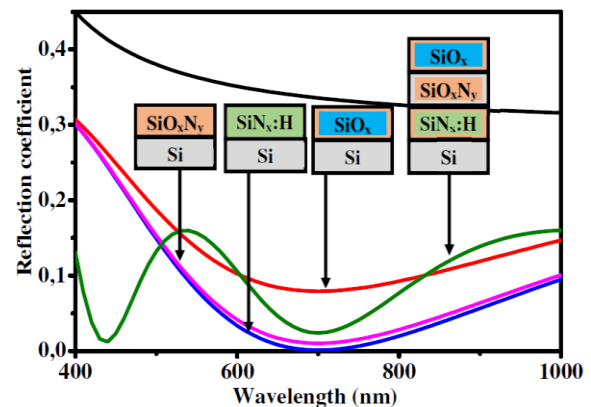
The reflection coefficient, as a function of the wavelength, is plotted for the following configurations:  $\text{SiO}_x/\text{Si}$ ,  $\text{SiO}_x\text{Ny/Si}$ ,  $\text{SiO}_x/\text{SiO}_x\text{Ny/Si}$ . The plots show an increase of reflection coefficient of  $\text{SiO}_x/\text{SiO}_x\text{Ny/Si}$  in wavelengths ranging around 700 nm. Lower values of reflection coefficient are obtained for 500 nm. From the analysis of these results, it is noted that the two single antireflecting layers show near zero reflectivity at the calibrated wavelength, at the contrary of the DARC configuration.



**Figure 6:** Reflection coefficient of silicon substrate with different anti-reflective coatings. The ARC thicknesses are calibrated for a wavelength  $\lambda = 700$  nm

The refractive indexes are  $n(\text{SiNx:H}) = 2$ ;  $n(\text{SiO}_x\text{Ny}) = 1.75$ ;  $n(\text{Si}) = 3.75$ .

The same analysis is obtained in Figure 6 showing the variation of the reflection coefficient of  $\text{SiO}_x\text{Ny/Si}$ ,  $\text{SiNx:H/Si}$ ,  $\text{SiO}_x\text{Ny/SiNx:H/Si}$ . Accordingly, the reflection coefficients are smaller at the calibrated wavelength for single layers than that of DCAR ones. The single antireflecting layers  $\text{SiNx:H/Si}$  and  $\text{SiO}_x\text{Ny/Si}$  allow a better photons flux transmission in the substrate and thus give higher cell efficiency than DCAR configuration.



**Figure 7:** Reflection coefficient of a multi antireflecting layer ( $\text{SiO}_x/\text{SiO}_x\text{Ny/SiNx:H/Si}$ ) as a function of incident light wavelength

Figure 7 shows a comparative study of the three single antireflecting layers with a multi antireflecting coating (MARC) composed with  $\text{SiO}_x/\text{SiO}_x\text{Ny/SiNx:H/Si}$ . As already analyzed in preceding paragraph, the variation of the reflectivity of three single antireflecting layers shows zero reflectivity at the calibrated wavelength. In addition, the MARC provides more zero reflectivities at 450 nm and 700 nm and thus gives a better transmission in a larger wavelength range.

## Conclusions

The work is focused on the influence of antireflecting coatings on silicon substrate optimization. It is shown that the  $\text{SiNx:H/Si}$  configuration gives lower reflectivity than those for  $\text{SiO}_x/\text{Si}$  and  $\text{SiO}_x\text{Ny/Si}$  and thus improve the short-circuit current. Therefore, the performance is altered for

DARC at the calibrated wavelength, the zero reflectivity being shifted to a lower value of wavelength (450 nm), proving that the photons flux transmission is increased in the ultraviolet range. A MARC, composed of three ARC, allows to enlarge the zero reflectivity wavelength range.

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